



Formation of Tungsten/Ammonium Perchlorate Composites and Their Reaction Kinetics

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Abstract: The reaction kinetics of tungsten nanoparticles/ammonium perchlorate (W/AP) composites, produced by a spray drying technique, were analyzed and compared with those of neat AP particles and aluminum nanoparticles/AP (Al/AP) composites. The W was found to raise the onset temperature of the thermal decomposition of AP by increasing the activation energy, whereas Al conversely lowered the onset temperature of AP due to the decreased activation energy. From the master plots of kinetic models with the experimental data, the Prout-Tompkins model and the 1-D diffusion controlled model were found to describe the low-temperature decomposition (LTD) and high-temperature decomposition (HTD), respectively, giving remarkable agreement with experimental curves for all heating rates. The presence of W was found to increase the HTD zone width compared with that of neat AP particles and Al/AP composites. Analysis of the average activation energy and pre-exponential factor showed that W increases the energy barrier and the frequency of occurrence of the reaction compared with that of neat AP particles at the LTD state, whereas W decreases both of them at the HTD state. The effect of Al was also shown to be similar to that of W, but the magnitudes of the variation in activation energy and the pre-exponential factor were relatively small.

Keywords: ammonium perchlorate, composite, thermal decomposition

1 Introduction

A great deal of attention has been paid to the compositions of ammonium perchlorate (AP) with metal nanoparticles (NPs) and metal oxide NPs being

used to improve the performance of AP. CuCo_2O_4 NPs were found to decrease the thermal decomposition temperature of AP, and the Fe_2O_3 NPs/AP composite showed a faster decomposition rate than that of neat AP [1, 2]. When employing Cu NPs, a decrease in activation energy of AP was observed [3]. These observations are closely related to the gas production of propellants and the thermal stability of the solid materials. For this reason, metal NPs or metal oxide NPs are mixed with AP particles as composite solid propellants [4].

To understand the effects of metal NPs or metal oxide NPs on the thermal decomposition of AP, the decomposition mechanism of AP needs to be clarified. The two different types of thermal decompositions of AP, low- and high-temperature decomposition, make identification of the reaction kinetics complicated [5]. Manelis *et al.* tried to investigate the thermal decomposition reaction of AP using a multistep kinetic model for the low-temperature decomposition [6]. Vyazovkin and Wight attempted to study the kinetics of thermal decomposition of AP by using the model-free isoconversional method, in which dependence of the effective activation energy on the extent of conversion was proposed [7]. On the other hand, Zhu *et al.* [8] tried to analyze the kinetics of thermal decomposition of AP with Al nanoparticles by employing various decomposition models.

In the 20th century, the catalytic effects of W on the oxidation of ammonia were specifically treated by Il'chenko *et al.* [9, 10]. Recently, the presence of W was found to increase the conversion of NH_3 to NO_x or N_2 [11]. This raises the potential of W/AP composites for enhancing gas emission. In the present article, we aim to find the reaction models that are suitable for describing the thermal decomposition of W/AP composites, including neat AP particles and Al/AP composites. Initially, the W/AP composites were produced by a spray drying system and their morphologies were identified by scanning electron microscopy (SEM) and transmission electron microscopy (TEM). Then, the effective activation energy was calculated by the model-free isoconversional method. Subsequently, based on the average activation energy, the mechanism of thermal decomposition of the W/AP composites was revealed by the model-fitting method, and then the pre-exponential factor of the kinetic parameters was determined, where the effect of W NPs on the thermal decomposition of AP was tackled in detail. Finally, we demonstrate the correctness of the selected kinetic models through comparison with the experimental curves for neat AP particles, W/AP and Al/AP composites.

2 Materials and Methods

2.1 Preparation

In the present work, AP (98.0%, Sigma Aldrich), 100 nm Al NPs (99.9%, Nano technology) and 100 nm W NPs (99.9%, Nano technology) were used. The surface of the Al and W NPs were fully protected by their oxide layers. Therefore, these NPs were not explosive. A schematic diagram of a spray drying system for the formation of the composites is illustrated in Figure 1. The AP (0.06 wt.)/methanol solution was prepared in a solution tank (Figure 1a). 1 wt.% of W or Al NPs, based on the AP, was mixed with the AP/methanol solution by mechanical stirring at 200 rpm. Fine droplets of the solution were produced by a two-fluid nozzle with N_2 gas. The N_2 gas pressure was fixed with 2 MPa. The atomized particles were rapidly dried in a reactor (Figure 1c) at 140 °C by a heat gun. The dried metal NPs/AP composites were filtered using a cyclone with a vacuum pump (ULVAC GCD-051X). To prevent explosion which may be caused by static electricity, the inner surface of the reactor was coated with polytetrafluoroethylene (PTFE), and the exposed metal parts were grounded.

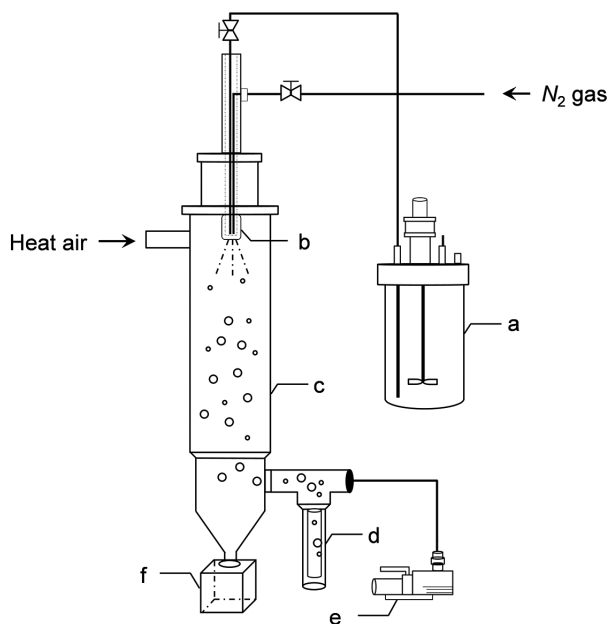


Figure 1. A schematic diagram of the spray drying system: a – solution tank, b – spray nozzle with two-fluids, c – reactor, d – cyclone, e – vacuum pump, and f – dust box.

2.2 Instrumentation

The size and morphology of the metal NPs/AP composites, after gold coating, were observed by SEM (JEOL JSM-7500F) with an accelerating voltage of 15 kV. The inner structure of the metal NPs/AP composites was investigated by high-resolution TEM (FEI Tecnai F20) operated at 200 kV. Analysis of the non-isothermal decomposition of the composites was performed with a thermogravimetric analyzer, TGA (Q600, TA Instrument), with heating rates of 5, 10, 20 and 30 °C/min in a nitrogen atmosphere at a flow rate of 100 mL/min. The samples, 5-16 mg, were accurately weighted into aluminum pans without seals.

2.3 Kinetic analysis

For non-isothermal kinetics, the rate of a solid-state reaction is written as [12]:

$$\frac{d\alpha}{dT} = \frac{A}{\beta} e^{-(E_a/RT)} f(\alpha) \quad (1)$$

where A is the pre-exponential factor, E_a is the activation energy, T is the absolute temperature, R is the ideal gas constant, $f(\alpha)$ is the differential reaction model (see Table 1), β is the heating rate, and α is the conversional fraction defined by:

$$\alpha = \frac{m_0 - m_t}{m_0 - m_\infty} \quad (2)$$

where: m_0 is the initial weight of the sample, m_t is the weight at time t , and m_∞ is the final weight.

Table 1. Differential and integral forms of the solid-state reaction models [12]

Model	Differential form $f(\alpha) = 1/k \, d\alpha/dt$	Integral form $g(\alpha) = kt$
Nucleation models		
power law (P2)	$2\alpha^{1/2}$	$\alpha^{1/2}$
power law (P3)	$3\alpha^{2/3}$	$\alpha^{1/3}$
Avrami-Erofeyev (A2)	$2(1-\alpha)[-\ln(1-\alpha)]^{1/2}$	$[-\ln(1-\alpha)]^{1/2}$
Avrami-Erofeyev (A3)	$3(1-\alpha)[-\ln(1-\alpha)]^{2/3}$	$[-\ln(1-\alpha)]^{1/3}$
Prout-Tompkins (B1)	$\alpha(1-\alpha)$	$\ln[\alpha/(1-\alpha)]+c$

Model	Differential form $f(\alpha) = 1/k \, d\alpha/dt$	Integral form $g(\alpha) = kt$
Geometrical contraction models		
contracting area (R2)	$2(1 - \alpha)^{1/2}$	$1 - (1 - \alpha)^{1/2}$
contracting volume (R3)	$3(1 - \alpha)^{2/3}$	$1 - (1 - \alpha)^{1/3}$
Diffusion models		
1-D diffusion (D1)	$1/(2\alpha)$	α^2
2-D diffusion (D2)	$-[1/\ln(1 - \alpha)]$	$((1 - \alpha)\ln(1 - \alpha)) + \alpha$

The differential form of Equation (1) was transformed by integration to:

$$g(\alpha) = \int_0^\alpha \frac{d\alpha}{f(\alpha)} = \frac{A}{\beta} \int_0^T e^{-(E_a/RT)} dT = \frac{A}{\beta} I(E_a, T) \quad (3)$$

where $g(\alpha)$ is an integral reaction model (Table 1). In the present work, the activation energy was calculated by the Vyazovkin method, and results in an effective activation energy [13].

$$\Phi = \sum_{i=1}^n \sum_{j \neq i}^n \frac{I(E_{a,\alpha}, T_{\alpha,i}) \beta_j}{I(E_{a,\alpha}, T_{\alpha,j}) \beta_i} \quad (4)$$

$$I(E_{a,\alpha}, T_\alpha) = \int_{T_\alpha - \Delta\alpha}^{T_\alpha} e^{-(E_{a,\alpha}/RT)} dT \quad (5)$$

where $I(E_{a,\alpha}, T_{\alpha,i})$ and $I(E_{a,\alpha}, T_{\alpha,j})$ are the exponential integrals at heating rates β_i and β_j , respectively. At a given α , the E_a is the value that minimizes Φ .

3 Results and Discussion

3.1 Morphologies of W/AP and Al/AP composites

The neat AP particles, W/AP and Al/AP composites prepared in the present work are shown in Figure 2. For the neat AP, the one micrometer-sized AP particles were found to aggregate as spherical shapes, which may be caused by rapid evaporation of the droplets. On the other hand, the particle sizes of W/AP or Al/AP were found to be larger than that of the neat AP particles due to heterogeneous nucleation by metal NPs. Figure 3 shows the particle size

distribution for the neat AP particles, and the W/AP and Al/AP composites, where their average sizes were estimated to be 0.8, 1.4, and 4.0 μm , respectively. The dispersion of the metal NPs in the AP crystals was confirmed by the TEM images (Figures 2d and 2e), where the metal NPs were not uniformly dispersed in the AP crystals, some of them being located on the crystal surfaces. Figure 4 shows the EDX spectrum of the W/AP and Al/AP composites. The presence of elements such as W, Al, O, and Cl is observed in the spectra.

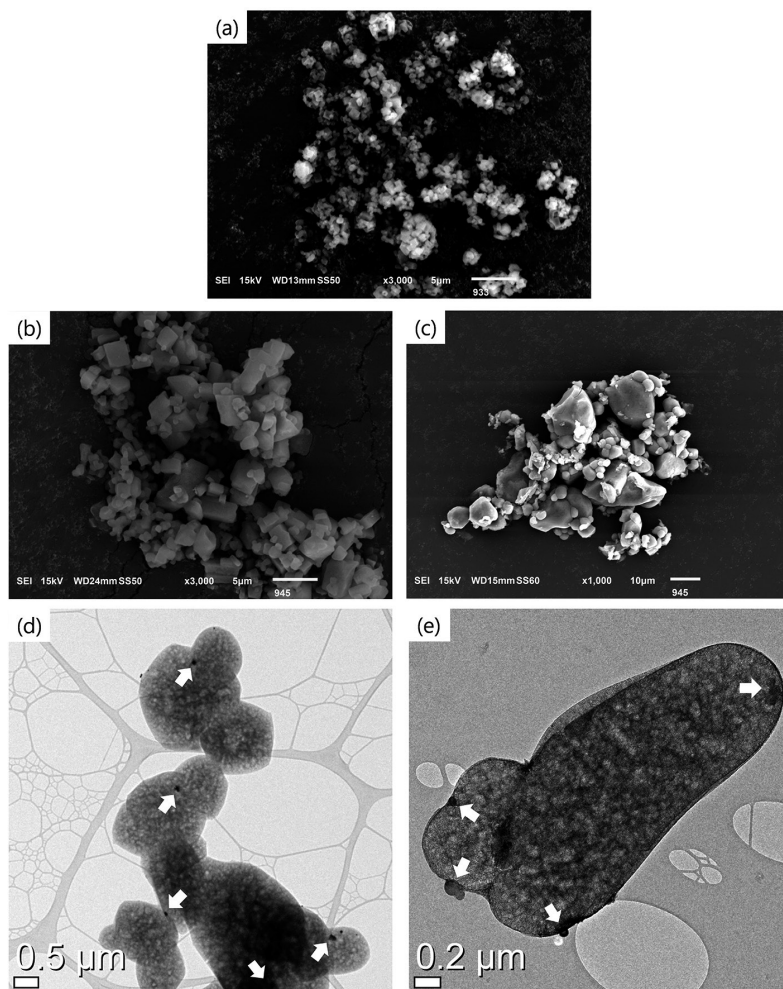


Figure 2. SEM images of (a) neat AP particles, (b) W/AP composite, and (c) Al/AP composite. TEM images of (d) W/AP composite, and (e) Al/AP composite. (The white arrows indicate the metal NPs).

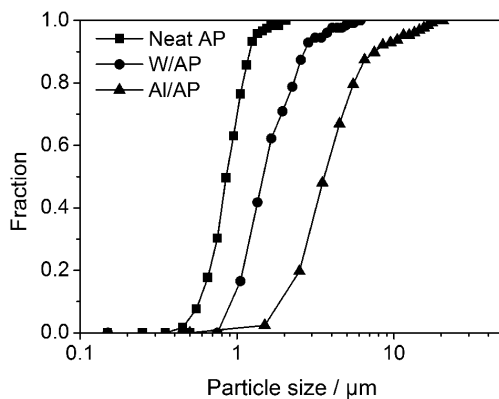


Figure 3. Cumulative particle size distribution of neat AP particles, and W/AP and Al/AP composites.

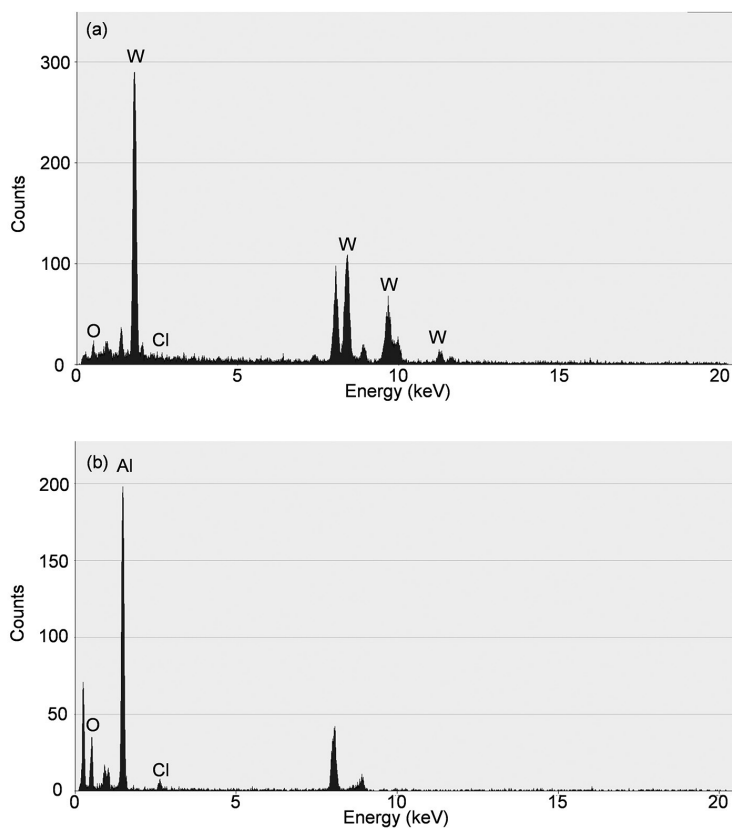


Figure 4. EDX data for (a) W/AP composite, and (b) Al/AP composite.

3.2 Analysis of TGA data

In general, the decomposition of AP was analyzed as a two step reaction: low-temperature decomposition (LTD, $<350\text{ }^{\circ}\text{C}$) and high-temperature decomposition (HTD, $>350\text{ }^{\circ}\text{C}$). In the present work, the inflection points were found to be close to 80, 92, and 76 wt.% for AP, W/AP, and Al/AP, respectively (Figure 5a-c). According to the mechanism of thermal decomposition of AP, the LTD state starts with proton transfer from NH_4^+ to ClO_4^- [14, 15]. From the crystal defects, such as dislocations, the gaseous products begin to form numerous nuclei and fill the cavities. However, as the nuclei reach a critical size, they stop growing when the pressure inside the cavity reaches 20 atm [16]. The main gaseous products of the LTD state are NH_3 , H_2O , N_2O , and O_2 [17]. In that case, it is known that about 30% of AP has decomposed and then the reaction ceases. On the other hand, at the HTD state, the chemical reaction takes place on the crystal surface, where the layer of gas phase is increased by the movement of $\text{NH}_3(\text{g})$ and $\text{HClO}_4(\text{g})$. In that case, decomposition and sublimation processes competitively interact, where energy is required to sublime the solid AP. The decomposition products include mainly HCl , H_2O , N_2O , NH_3 , Cl_2 , NO , O_2 , NO_2 , and ClO_2 [17].

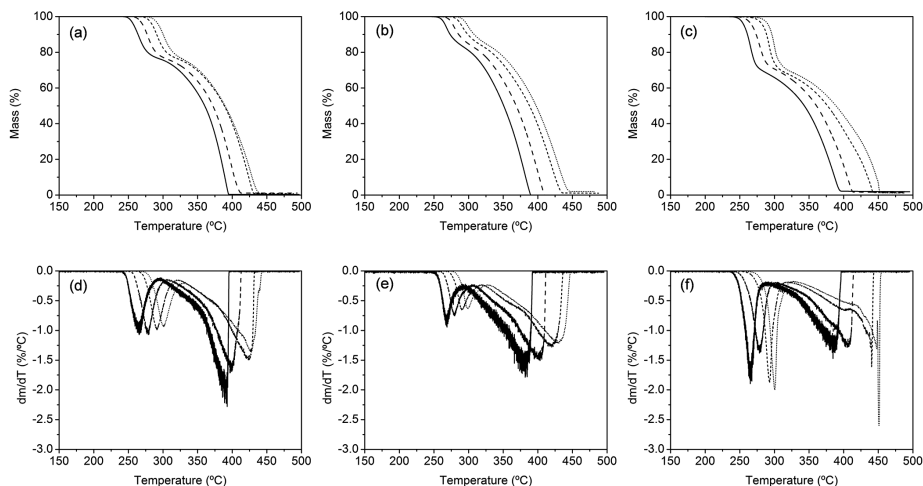


Figure 5. TG curves of (a) neat AP particles, (b) W/AP composite, and (c) Al/AP composite, for all heating rates. DTG curves of (d) neat AP particles, (e) W/AP composite, and (f) Al/AP composite for all heating rates; (solid line: $5\text{ }^{\circ}\text{C}/\text{min}$, dashed line: $10\text{ }^{\circ}\text{C}/\text{min}$, short dashed line: $20\text{ }^{\circ}\text{C}/\text{min}$, dotted line: $30\text{ }^{\circ}\text{C}/\text{min}$).

In this present work, the onset temperature is defined as the point where the weight of material begins to be decomposed, $\alpha = 0.02$. From Table 2, the onset

temperature was found to be shifted by the presence of metal NPs. Al NPs are shown to decrease the onset temperature of the LTD reaction, whereas W NPs increases the onset temperature of the LTD reaction. The reason behind the difference in onset temperatures is the relative magnitude of the activation energies. Figure 6 represents the variation of E_a as a function of degree of conversion, α , determined by the isoconversional method for non-isothermal TG data. The presence of metal NPs was found to change the distribution of the activation energies. Theoretically, the $E_a(\alpha)$ implies the energy barrier required for reaction from the previous point $\alpha - \Delta\alpha$, to the present point α . At $\alpha = 0.02$, the E_a of the W/AP composite, 144.0 kJ/mol, is larger than the E_a of neat AP particles, 120.6 kJ/mol, whereas the E_a of the Al/AP composite, 89.5 kJ/mol, is smaller than that of neat AP particles. Therefore, it can be understood that the decreased E_a of Al/AP composites promotes the LTD state, whereas the increased E_a of W/AP composites retards the LTD state. Interestingly, the points of the LTD termination correspond approximately to the points, $\alpha = 0.22$ (neat AP), 0.10 (W/AP), and 0.26 (Al/AP), respectively, where the E_a starts to increase dramatically.

Table 2. Onset temperature of the thermal decomposition of neat AP particles, W/AP composite, and Al/AP composite

Heating rate, β , [°C/min]	Onset temperature, [°C]		
	neat AP	W/AP	Al/AP
5	240.1	252.3	232.2
10	246.7	256.8	238.3
20	263.5	266.0	256.3
30	268.4	280.2	264.6

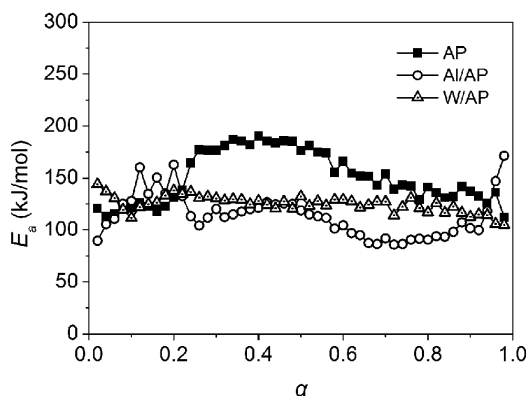


Figure 6. Variation of the effective activation energy determined by the isoconversional method.

Furthermore, the existence of metal NPs was found to affect considerably the LTD zone width. For the neat AP particles, 20 wt.% of AP was decomposed in the LTD state, whereas in the presence of W only 8 wt.% of AP was decomposed in the LTD state. However, in the case of the Al/AP composite, the LTD state was expanded to 24 wt.%. From the fact that the LTD reaction is hindered by the adsorption of NH_3 gas on the AP crystal surfaces, the different effects of the metal NPs on AP may be surmised as follows. Metal NPs containing many defects have the potential to capture the gaseous products from AP [18]. Therefore, the concentration of NH_3 on the metal NPs/AP interfaces increases and accordingly the LTD reaction tends to be terminated. Furthermore, the metal NPs existing within the AP could increase the dislocation density. The creation of dislocations and their movement can promote the accumulation of products in the nucleus and slowing of the LTD reaction ensues [19]. On the other hand, metal NPs could stimulate the thermal decomposition of AP because the surface-located electrons of molecules are attracted by the metal and consequently chemical bonds are broken [20]. The former would decelerate the thermal decomposition, whereas the latter would accelerate it. From this point of view, the difference in the LTD zone width for the W/AP and Al/AP composites may be derived from the different mechanisms that occur competitively.

3.3 Solid-state kinetic analysis

3.3.1 Neat AP

Based on the effective activation energy, model-fitting was performed to find the reaction model for thermal decomposition of neat AP particles, and W/AP and Al/AP composites. At the LTD state, nucleation models such as P2, P3, A2, A3 and B1 were employed because the nucleation of gaseous products occurs inside the AP crystals [21]. On the other hand, at the HTD state, the nucleation occurs markedly on the surface [5], which leads to a reaction controlled by crystal shape and mobility of the gas phase. For this reason, the geometrical contraction models (R2 and R3) and the diffusion models (D1 and D2) were employed. In this work, the E_a values were shown to not be significantly changed with respect to α for each of the LTD and HTD states, where the E_a was roughly constant over each range and the difference between the maximum and minimum values of E_a were smaller than 20 - 30% of the average E_a . Therefore, it is reasonable to employ two single reaction models for each state [22].

To explore the reaction model which was most suitable for describing the thermal decomposition processes, the master plot of $g(\alpha)/g(0.5)$ against α was evaluated from the experimental data and different heating rates for each reaction model. Based on the average E_a of the LTD state and of the HTD state,

121.49 kJ/mol ($0.00 < \alpha < 0.20$) and 157.45 kJ/mol ($0.20 < \alpha < 1.00$), respectively, the experimental master plots were obtained as shown in Figure 7. In this figure, all values were separately normalized for each state. To check the correctness of the selected models, the deviation, σ , of the master plots between a selected model and the experimental curves was introduced as follows:

$$\sigma = \sqrt{E \left[\sum_{i=1}^n \left(g(\alpha_{N,exp,i}) / g(0.5_{N,exp,i}) - g(\alpha_{N,mod}) / g(0.5_{N,mod}) \right)^2 / n \right]} \quad (6)$$

where the subscripts N , exp and mod , denote the normalized, experimental, and reaction model, respectively, E and n represent the mean and the number of experiments, respectively.

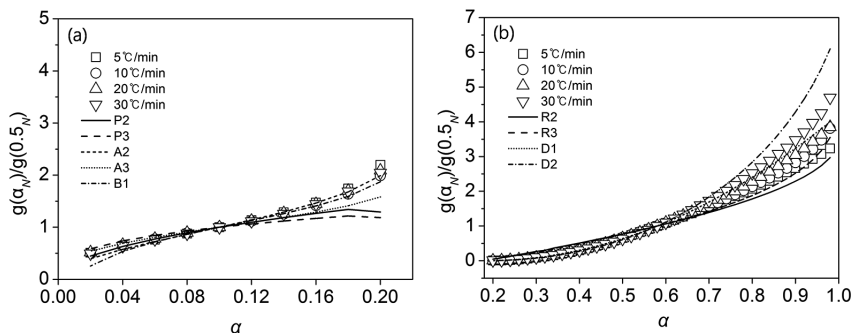


Figure 7. Master plots of the experimental data and the reaction models for neat AP particles: (a) P2, P3, A2, A3, and B1 at $0.00 < \alpha < 0.20$; (b) R2, R3, D1, and D2 at $0.20 < \alpha < 1.00$.

In Table 3, the A2 and B1 models are shown to exhibit small deviations in the LTD state, and accordingly they seem to follow exactly the trends of the LTD state as shown in Figure 7a. However, the ambiguity of a selected reaction model still remains when performing the model-fitting method without experimental observation. In practice, it is difficult to discriminate between the Avrami-Erofeyev (A2, A3) and Prout-Tompkins (B1) models due to their similar sigmoidal trend of the solid state reaction and the narrow domain of the LTD state. This exacerbates identification of the process for thermal decomposition of AP.

Nuclei formation processes have been reported to be localized in the screw and edge dislocations inside crystals in an experimental study on the nucleation of AP [23, 24]. Nucleation does not occur randomly over the whole crystal volume but originates from dislocations. Once nucleation occurs near existing

dislocations, the AP crystal is deformed by increased pressure and leads to the formation of new dislocations [25, 26]. The density of newly generated dislocations was found to be larger near the nucleus rather than near unreacted AP [27]. In this way, the kinetics of thermal decomposition of AP in the LTD state is similar to the autocatalysis of the B1 model proposed by Prout and Tompkins. Consequently, the Avrami-Erofeyev model developed for describing random nucleation processes appears to be insufficient for describing the LTD state of AP. For this reason, the B1 model was selected as the reaction model in the LTD state. On the other hand, the D1 model was selected as the reaction model in the HTD state, providing the best fit for the experimental master plots of AP, with the lowest deviations, as given in Table 3 and Figure 7b.

Table 3. Deviation (σ) of the master plots for neat AP particles

LTD ($0.00 < \alpha < 0.20$)		HTD ($0.20 < \alpha < 1.00$)	
Model	σ	Model	σ
P2	0.2824	R2	0.4244
P3	0.3403	R3	0.3099
A2	0.0621	D1	0.1983
A3	0.3400	D2	0.7186
B1	0.1191		

The pre-exponential factors were obtained from Equation (3), where A was determined from the slope of the $g(\alpha)$ vs. $I(E_a, T)/\beta$ plot at various heating rates by the method of linear least square fitting. The values of A for the LTD and HTD states were $5.13 \times 10^{11}/\text{min}$ and $4.07 \times 10^{11}/\text{min}$, respectively. Figure 8 shows the reconstructed curves for all heating rates based on the average E_a and A . The predicted plots for AP were shown to give good agreement with the experimental data. It seems that the combination of two single reaction models, B1 and D1, are suitable for describing the thermal decomposition of AP. Experimentally, the LTD reaction ceases due to accumulation of the gaseous products which are mainly generated near the dislocations of AP. Hence, it markedly follows the B1 model. On the other hand, the HTD state is governed by mass transfer that competes with sublimation [7]. The adsorption of gaseous products on the AP crystal surfaces is a reaction-limiting factor of AP that hinders diffusion of the gaseous products from the reaction sites. Furthermore, the diffusion is also hampered by the crystal lattice of AP, through which gaseous products should permeate. Therefore, the thermal decomposition of AP at the HTD state seems to follow the D1 model due to restriction of the motion of gaseous products.

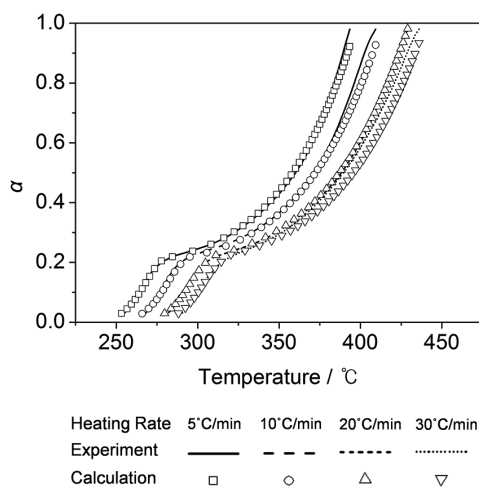


Figure 8. The experimental and reconstructed curves for neat AP particles.

3.3.2 *W/AP*

As with the analysis of neat AP particles, the average E_a values of the W/AP composite for the LTD and HTD states were obtained as 132.78 kJ/mol ($0.00 < \alpha < 0.08$) and 124.04 kJ/mol ($0.08 < \alpha < 1.00$), respectively. Compared with the E_a values for neat AP particles, the presence of W was shown to increase the average E_a in the LTD state. The elevated activation energy in the LTD state implies that a relatively high potential barrier is imposed on the nucleation process for AP particles and therefore nucleation near the W NPs could be hindered. Moreover, the presence of W NPs enables the E_a of AP particles to decrease continuously to $\alpha = 0.08$, whereas the E_a of neat AP particles increases continuously to $\alpha = 0.12$, and then drastically decreases to $\alpha = 0.16$. The declining tendency of the activation energy is one of the distinctive characteristics of the W/AP composite. This seems to be significantly associated with the LTD zone width, which is narrower compared to neat AP particles.

In Figure 9, the A3 and B1 models are shown to provide a good fit to experimental data in the LTD state, whereas only the D1 model exclusively follows the experimental data in the HTD state. The deviations of the master plots helped us to determine the reaction model. In the present work, the A3, B1 and D1 models were found to have smaller deviations in the experimental master plots, as can be seen from Table 4.

Employing the B1 and D1 models in the LTD and HTD states, respectively, the pre-exponential factors were obtained as $1.05 \times 10^{13}/\text{min}$ and $1.09 \times 10^9/\text{min}$.

Figure 10 shows that the reaction model accurately predicts the experimental curves of the W/AP composite at all heating rates, where a mechanism change in the thermal decomposition of AP is well developed. Fundamentally, $\exp(-E_a/RT)$ is the fraction of the bond redistribution step that has occurred to convert reactants into products, and A is the frequency of occurrence of the reaction [28]. Hence, the product of A and $\exp(-E_a/RT)$ becomes a rate constant for determining the total reaction rate. In this work, the frequency of occurrence A of the W/AP composite was found to be larger than that of neat AP particles. However, as shown in Figure 5, the magnitude of da/dT of the W/AP composite is generally smaller than that of neat AP particles in the LTD state (250-290 °C). This implies that decomposition of the W/AP composite is slower than that of neat AP particles at a given heating rate. In that case, the reason is mainly due to a very high activation energy of the W/AP composite, which drastically decreases the fraction of occurrence of the bond redistribution step and cancels out to a large extent the effect of A on the reaction. On the other hand, the W/AP composite decomposes more rapidly than neat AP particles in the HTD state (320-420 °C), even though the frequency of occurrence A of the W/AP composite is much lower than that of neat AP particles. In that case, a very large fraction of the bond redistribution step originating from a considerably decreased activation energy E_a offsets a low frequency of occurrence A .

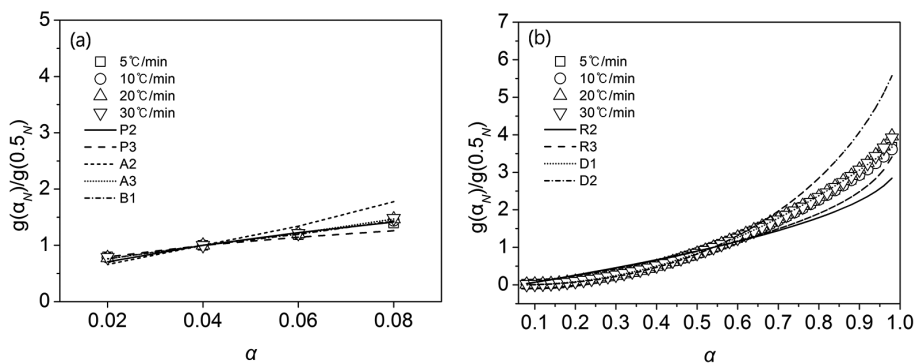
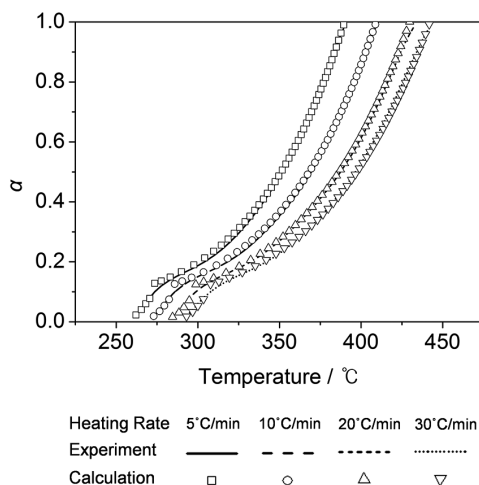


Figure 9. Master plots of experimental data and reaction models for the W/AP composite: (a) P2, P3, A2, A3, and B1 at $0.00 < \alpha < 0.08$; (b) R2, R3, D1, and D2 at $0.08 < \alpha < 1.00$.

Table 4. Deviation (σ) of the master plots for the W/AP composite

LTD ($0.00 < \alpha < 0.08$)		HTD ($0.08 < \alpha < 1.00$)	
Model	σ	Model	σ
P2	0.0473	R2	0.3977
P3	0.0986	R3	0.2749
A2	0.1901	D1	0.0534
A3	0.0254	D2	0.5436
B1	0.0220		

**Figure 10.** The experimental and reconstructed curves for the W/AP composite.

3.3.3 Al/AP

From the variation of E_a in Figure 6, the average values of E_a for the LTD and HTD states were 127.98 kJ/mol ($0.00 < \alpha < 0.24$) and 108.83 kJ/mol ($0.24 < \alpha < 1.00$), respectively. Compared with neat AP particles, the presence of Al NPs was found not only to increase the average E_a in the LTD state, but also to decrease the average E_a in the HTD state. These results are similar to the case of the W/AP composite, in which a relatively high potential barrier is imposed on the process of nucleation. From Figure 11, the A3 and B1 models were found to accurately mirror the experimental curves in the LTD state, whereas there is ambiguity between R3 and D1 in the HTD state. In this work, the B1 model was selected as the reaction model of the LTD state and D1, with the lowest deviation (Table 5), was selected in the HTD state. Based on these reaction models, B1 and D1, and the average E_a , the pre-exponential factors A for the LTD and HTD states were estimated as $5.03 \times 10^{12}/\text{min}$ and $5.21 \times 10^7/\text{min}$, respectively.

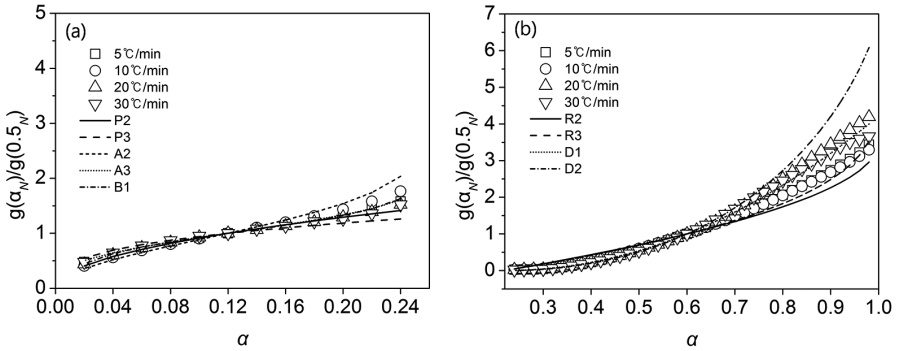


Figure 11. Master plots of experimental data and reaction models for the Al/AP composite: (a) P2, P3, A2, A3, and B1 at $0.00 < \alpha < 0.24$; (b) R2, R3, D1, and D2 at $0.24 < \alpha < 1.00$.

Table 5. Deviation (σ) of the master plots for the Al/AP composite

LTD ($0.00 < \alpha < 0.24$)		HTD ($0.24 < \alpha < 1.00$)	
Model	σ	Model	σ
P2	0.0791	R2	0.4306
P3	0.1441	R3	0.3265
A2	0.1833	D1	0.2018
A3	0.0523	D2	0.7501
B1	0.0501		

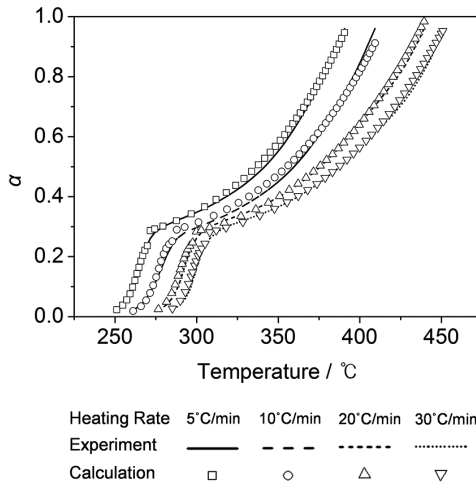


Figure 12. The experimental and reconstructed curves for the Al/AP composite.

Figure 12 shows the reconstructed curves of the B1 and D1 models for each state that accurately follow the experimental curves. Consequently, the calculated kinetics parameters, such as E_a and A , were found to be suitable for describing the thermal decomposition of the Al/AP composite. The presence of metal NPs yields a large value of A in the LTD state, whereas it provides a smaller value of A in the HTD state. However, the Al NPs have a diametrically opposite effect on the reaction rate compared to the W NPs. In Figure 5, the magnitude of $d\alpha/dT$ of the Al/AP composite was found to be larger than that of neat AP particles in the LTD state (250-290 °C). In that case, a high frequency of occurrence A in the Al/AP composite exceeds a low fraction originating from a high activation energy, so that the Al/AP composite decomposes more rapidly than neat AP particles. On the other hand, the Al/AP composite decomposes more slowly compared to neat AP particles in the HTD state (320-420 °C), where the fraction of occurrence of the bond redistribution step originating from the lower E_a cannot offset a very low frequency of occurrence A .

4 Conclusions

In the present work, the effect of tungsten nanoparticles on the thermal decomposition of AP was quantitatively identified by using the isoconversional method and reaction models suitable for describing the thermal kinetics. At the degree of conversion, $\alpha=0.02$, the activation energy of the W/AP composite was found to be larger than that of neat AP particles, and led to the delay of the LTD state. On the other hand, the Al/AP composite exhibits advanced decomposition due to the low activation energy compared with neat AP particles. The W NPs were found to expand the HTD zone width compared to neat AP particles, whereas the Al NPs conversely affect the LTD zone width. In practical terms, the HTD of AP is important because its temperature range is in the combustion zone of composite propellants [29], and a larger amount of gaseous products is produced from one mole of AP than at the LTD zone [30]. In this respect, the W NPs/AP composite may improve the performance of AP-based composite solid propellants by increasing the HTD zone width.

Using the model-fitting method combined with the master plot, it was found that the Prout-Tompkins model and 1-D diffusion controlled model could reproduce the experimental curves with high accuracy. These give a good explanation for autocatalytic nucleation in the LTD zone and diffusion controlled reaction in the HTD zone, respectively. In this work, the W NPs and Al NPs increase the activation energy, E_a , and the pre-exponential factor, A , in the LTD

state, whereas they decrease both parameters in the HTD state. However, the W/AP and Al/AP composites were found to exhibit different behaviour. The W/AP composite showed a tendency for the decomposition rate to be dominated by the fraction of occurrence of the bond redistribution step originating from the activation energy E_a rather than the frequency of occurrence A . On the other hand, a decomposition rate of the Al/AP composite appeared to be affected by the frequency of occurrence A to a larger extent, and the effect of E_a became relatively smaller.

The model-fitting method combined with an isoconversional method was shown to give a good explanation for the effect of W NPs on the thermal decomposition of AP. However, it should be kept in mind that, although the LTD and HTD states were found to be described by the Prout-Tompkins model and the 1-D diffusion model with high accuracy, this does not mean that the thermal decomposition of AP must take place only by these two consecutive reactions, which are essential in these reaction models. Nevertheless, they offer a key clue to the reaction model that significantly dominates the thermal decomposition of AP, and that the kinetic analysis is sufficiently adequate to accomplish support for the experimental observations. Consequently, the kinetic parameters that are obtained here allow an understanding of the decomposition behaviour of the W/AP composite compared with that of neat AP particles and Al/AP composites.

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